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CALCULATION OF AIR ION REGIME IN THE CASE OF ARTIFICIAL AIR IONIZATION

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Summary. Purpose. One of the major tasks in the field of labor protection is providing of the necessary qualitative composition of air in the working areas of office and industrial spaces. In order to maintain the necessary air ion level in the air space premises, the artificial ionization of air is used often in the premises. At present in Ukraine analytical model are used for the calculation of air ion regime in premises, influencing on the formation process of air ions concentration field. An alternative solution is the use of CFD models, developing including the air jets aerodynamics in the premise, the presence of furniture, equipment, transfer of ions under an electric field, and other physical factors, determining intensity and shape of air ions concentration field in the premise. **Methodology.** Influence of air flow was taken into account in the development of CFD models for calculation of air ion regime in the apartment, caused by operation of ventilation, diffusion, electric field impact, as well as the interaction of different polarity ions with each other, and their interaction with dust particles. The proposed model of calculation of air ion regime in premises based on the use of aerodynamics, electrostatics and mass transfer levels. This model allows operatively to calculate air ions concentration field with the influence of the walls, floor, ceiling and obstacles on the process of air ions dispersion, the specific location of different polarity ions emission and their interaction in the premise and work areas in conditions of artificial air ionization. **Results.** The calculated data were obtained and on their base could be estimated the concentration of air ion anywhere in the premise with artificial air ionization. Ions concentration field, being calculated using this CFD model, as concentration field isolines is presented. **Originality.** The results of the air ion regime calculation in the premise are presented, based on numerical 2D CFD model. To solve the problem on the base, of the developed CFD model, about a minute of computer time is required. **Practical value.** 2D CFD model for air ion regime calculation in premises allows to calculate the ions concentration in their working areas of premise in conditions of artificial air ionization including the basic physical factors, determining the formation of ions concentration fields.

Key words: CFD model; air ion regime; concentration field of air ions, artificial ionization

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Introduction. Under modern conditions one of the most important tasks in the labor protection field is to provide of proper micro-climatic conditions for the staff of industrial and office premises [2-12]. One of the significant parameters is directly affecting on the

staff productivity is the qualitative composition of the air. In order to maintain the necessary ions level in the air space is used often the artificial ionization of the indoor air. Ionization is generally carried out either by setting the ionizer indoors or supply of ionized air into the room. In the case

of an ionized air supply it is necessary to calculate the level of negative ions in the working areas of office and industrial premises, and therefore have the necessary mathematical apparatus for calculating the ions concentration field in the premises. It is important to take into account all factors that influence the ions dispersion in the room.

In Ukraine today for calculating air ion regime in premises mainly used analytical models [4-12], allowing calculating the ions concentration in the room. However, as a rule, in these models do not consider the aerodynamics of the air jets in the room, the presence of equipment, furniture, dust emission sources, that is, physical factors influencing the formation of ions concentration field. To account for the above mentioned factors, it is more expedient to use CFD models [2; 3; 13; 16].

Purpose. In the given work results of applying CFD numerical models, which is taken into account the placement of furniture and equipment in the room and physical factors determining the formation of the ions concentration field, for computation air ion regime in premises and in work areas in the conditions of artificial air ionization.

Methodology. In the development of a numerical model for computation of air ion regime should take into account the impact of indoor air flows caused by the ventilation operation, diffusion, electric field effects. It is also necessary to take into account the interaction of different polarities ions with each other and their interaction with the dust particles. Thus, in the simulation of air ions dispersion to account for the above processes will use the transfer equation in the form [16]:

$$\begin{aligned} \frac{\partial C}{\partial t} + \frac{\partial(u + bE)C}{\partial x} + \frac{\partial(v + bE)C}{\partial y} = \\ = \frac{\partial}{\partial x} \left(\mu_x \frac{\partial C}{\partial x} \right) + \frac{\partial}{\partial y} \left(\mu_y \frac{\partial C}{\partial y} \right) - CB - \\ - SCD + \sum Q(t) u(x-x_i) v(y-y_i), \quad (1) \end{aligned}$$

where C, B, D – the concentration of negative and positive air ions and dust particles respectively; u, v – velocity components of airflow in the room; $\mu = (\mu_x, \mu_y)$ – diffusion coeffi-

cients; t – time; r – the rate recombination of ions with different polarity; s – the rate of recombination of ions with dust particles; Q_{Ci} – the intensity of the negative ions emission at the appropriate points with the coordinates x_c, y_c ; $u(x-x_i)u(y-y_i)$ – Dirac delta function; b – coefficient of ion mobility; E – electric field intensity.

Since air ions have a charge, they generate an electric field E , which is described by the following equation [16]:

$$\frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} = \frac{q_e}{V_0}, \quad (2)$$

where V_0 – the dielectric permittivity; q_e – the space charge density.

From equation (2) can go to the scalar potential, taking into account such dependence

$$E_x = -\frac{\partial w}{\partial x}, \quad E_y = -\frac{\partial w}{\partial y}. \quad (3)$$

Then we get the Poisson equation of the following form [16], which we will use to simulate the electric field:

$$\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} = -\frac{q_e}{V_0}, \quad (4)$$

where $q_e = -eC(x, y)$, $C(x, y)$ – the concentration of negative air ions; w – scalar potential; e – elementary charge. On the basis of this equation is performed simulations of the electric field.

To describe the processes of positive ions and dust dispersion will use the equation of transfer in the form [16]:

$$\begin{aligned} \frac{\partial B}{\partial t} + \frac{\partial uB}{\partial x} + \frac{\partial vB}{\partial y} = \frac{\partial}{\partial x} \left(-\frac{\partial B}{\partial x} \right) + \\ + \frac{\partial}{\partial y} \left(-\frac{\partial B}{\partial y} \right) - rCB - SBD + \\ + \sum Q(t) u(x-x_i) v(y-y_i), \quad (5) \end{aligned}$$

$$\begin{aligned} \frac{\partial D}{\partial t} + \frac{\partial uD}{\partial x} + \frac{\partial vD}{\partial y} = \\ = \frac{\partial}{\partial x} \left(-\frac{\partial D}{\partial x} \right) + \frac{\partial}{\partial y} \left(-\frac{\partial D}{\partial y} \right) + \\ + \sum Q_{Di}(t) u(x-x_D) v(y-y_D). \quad (6) \end{aligned}$$

Designation of the physical parameters in these equations is the same, which was given for the equation (1).

To calculate the aerodynamics of air flow in the room will use a model of potential flow. In this case the Laplace equation for the velocity potential is a modeling equation

$$\frac{\partial^2 P}{\partial x^2} + \frac{\partial^2 P}{\partial y^2} = 0, \quad (7)$$

where P – velocity potential.

The components of the air environment velocity vector are connected with the velocity potential following dependencies

$$u = \frac{\partial P}{\partial x}, \quad v = \frac{\partial P}{\partial y}. \quad (8)$$

Formulation of boundary conditions for the modeling equations is considered in [1; 13; 16].

For the numerical integration of the transfer equations [1; 11; 13; 16] used the implicit alternately - triangular difference schemes, which has been implemented by the method of running accounts [1]. For the numerical solution of the Laplace equation and Poisson's equation used the Libman's method. The calculation is performed on rectangular difference grid.

On the basis of the difference schemes was designed the software package (code) «ION-2». This package is built on a modular principle; each sub-program implements a specific numerical integration of the modeling equation and implementing appropriate boundary conditions.

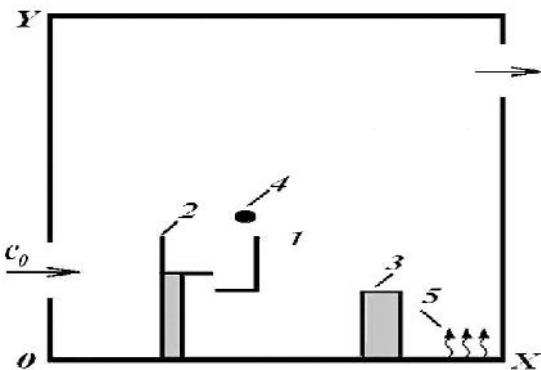


Fig. 1. The computational domain: 1 – chair; 2 – work desk; 3 – rack; 4 – place of positive ions emission (the position of the respiratory organs); 5 – place of dust emission

A feature of the modeled process is the presence of furniture in the room, i.e., objects, influencing the formation of ion concentration field. To «reproducing» these and other ob-

jects in the numerical model uses a technology called «porosity technique», also called the method of marking [1]. The essence of this technology lies in the encoding of difference cells, which belong to such facilities, and the implementation of them in the appropriate boundary conditions.

Findings. CFD numerical model was used to calculate the negative ions concentration in the field of office space in the conditions of artificial air ionization.

Sketch of the computational domain is shown in Fig. 1. It is the premises where to the air flows enter through the ventilation system. These air contains negative ions with a concentration $C_0=0.55\times10^{11}$ particles/m³. The air exit from the room occurs through the outlet in the wall. The work area includes table and chair placed next.

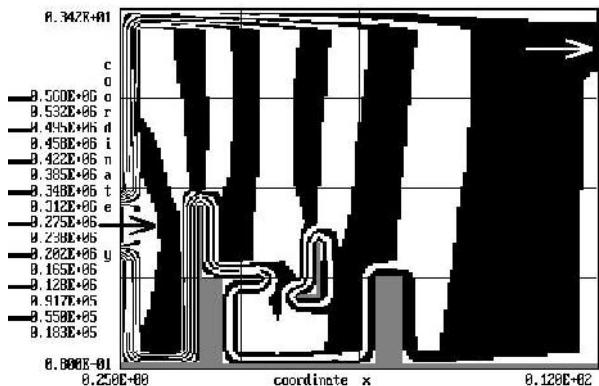


Fig. 2. Concentration field of negative air ions in the room

The people are the source of positive ions emission in the room. Therefore in the zone of their respiratory organs (Fig. 1, pos. 4) set point sources of positive ions emission intensity $Q_B = 7\times10^5$ particles/s. The other of the problem parameters are: the size of the computational domain 12.25m×3.50m; ventilation rate is equal 3 [1/h]; the position of the inlet and outlet ventilation holes shown by arrows in Fig. 1; $= 1.5\times10^{-12}$ m³/s, $= 1\times10^{-12}$ m³/s [13; 16]; the coefficients of turbulent diffusion in all directions are taken to equal $\sim_x = \sim_y = kV$ (where $k = 0.1$ – the parameter, V - the local velocity in the specific computational point and it is defined by solving the aerodynamic problem). Dust emission occurs indoor, $Q_{Di}=52\times10^6$ particles/s (dust emission position shown in Fig. 1 as a

wavy line). Purpose of numerical modeling is definition of the negative ions concentration in the room and the area of the human respiratory system.

The results of numerical simulation on the following figures are shown. On these figures the negative ions concentration field in the room was given. The simulation results are given in dimensionless form, where each number is a measure of concentration in percentage of the maximum ions concentration in the room C_{max} . Printing was done on the format as «whole number», i.e. the fractional part shall not be issued to the printer.

In Fig. 2, the concentration of negative ions in the room is presented. The concentration of negative ions above the chair (the position of head of the worker) is equal to 0.021×10^{12} particles/m³. It is known that the maximum level of negative ions in the working areas must be 0.05×10^{12} particles/m³. So, for the proposed regime of ionization the con-

centration of negative ions is satisfied this condition.

In conclusion, for the solution of the problem on the basis of the developed CFD model it took about 1 minute of computer time.

Originality and practical value. The results of the new CFD model for the computation of air ion regime in rooms with artificial air ionization are represented. This 2D CFD model is based on the use of aerodynamics, electrostatics and mass transfer equations, and developed taking into account the main factors determining the formation of fields of concentration of ions in the room and work areas.

Conclusions. The article contains results numerical simulation of air ion regime in office and industrial environments with artificial air ionization. Calculated ions concentration field in the room, presented in the form of isolines. To solve the problem on the basis of the developed CFD model took about a minute of computer time.

REFERENCES

1. Beliaev N.N., Hunko E.Yu. and Rostochilo N.V. *Zashchita zdaniy ot proniknoveniya v nikh opasnykh veshchestv* [Protection of building from penetration of hazardous substances into them]. Dnipropetrovsk: Aktsent PP, 2014, 136 p. (in Russian)
2. Beliaev N.N. and Tsygankova S.G. *Otsenka aeroionnogo rezhima v rabochikh zonakh na baze CFD modeli* [Evaluation of air ion regime in work areas on the base of CFD models] *Zbirnyk naukovykh prats NGU* [Proceedings of NMU]. 2015, no. 46, pp. 168-173. (in Russian).
3. Beliaev N.N. and Tsygankova S.G. *Raschet aeroionnogo rezhima v pomeshchenii i v rabochey zone na baze chislennoy modeli* [Calculation of air ion regime in the premises and work area on the basis of a numerical model] *Zbirnyk naukovykh prats NGU* [Proceedings of NMU]. 2015, no. 47, pp. 137-143. (in Russian).
4. Glyva V.A., Klapchenko V.I., Ponomarenko S.M., Shevchenko L.O and Smakovskiy D.S. *Vyznachennia ta prognozuvannia dynamiky zminy aeroionnogo skladu povitria vyrobnychyh prymishchen* [Determination and prediction of the ionic air composition change dynamics in industrial premises]. *Visnyk natsionalnoho tekhnichnogo universitetu Ukrayiny «Kyivskyi politekhnichnyi instytut»* [Bulletin of National Technical University of Ukraine «Kyiv Polytechnic Institute】. 2010, iss. 19, pp. 161-168. (in Ukrainian).
5. Tolkunov I.A., Mariniukh V.V., Popov I.I. and Ponomar V.V. *Deiaki aspeky zabezpechennia normatyvnogo aeroionnogo rezhymu robochoho seredovishcha prymishchen spetsialnogo pryznachennia MNS Ukrayiny* [Some aspects of the regulatory ionic regime of working environment of the special purpose premises of the Ministry of Emergencies of Ukraine]. *Problemy nadzvychainykh sytuatsiy* [Problems of Emergencies]. 2008, iss. 8, pp. 198-206. (in Ukrainian).
6. Zaporozhets O.I., Glyva V.A. and Sidorov O.V. *Normuvannia aeroionnogo skladu povitria robochykh prymishchen ta osnovni napriamy yogo vdoskonalennia* [The standardization of the air ionic composition of work premises and main directions of its improvement]. *Visnyk natsionalnogo aviationsonnogo universytetu* [Bulletin of national aviation university]. 2011, vol. 46, no. 1, pp. 139-143. (in Ukrainian).
7. Zaporozhets O.I., Glyva V.A. and Sidorov O.V. *Printsypy modeliuvannia aeroionnogo skladu povitria u prymishchenniakh* [The principles of modeling of the air ionic composition in premises]. *Visnyk natsionalnogo aviationsonnogo universytetu* [Bulletin of National Aviation University]. 2011, vol. 47, no. 2, pp. 120-124. (in Ukrainian).
8. Levchenko L.O., Glyva V.A. and Sidorov O.V. *Tryvymirne modeliuvannia prostorovykh rozpodiliv kontsentratsii aeroioniv u povitri* [Three-dimensional modeling of air ions concentrations spatial distributions on air]. *Upravlinnia rozvytkom skladnykh system* [Control of the development of complex systems]. 2012, iss. 11, pp. 198-206. (in Ukrainian).

9. Bahrushyn V.E., Ignakhina M.A., Vertinskii D.V. and Yeevsiukov A.Yu. *Modelirovanie raspredeleniya kontsentratsii ionov v blizi ionizatora* [Simulation of distributing concentration of ions nearly ionizer]. *Skladni systemy ta protsesy* [Complex systems and processes]. 2002, no. 1, pp. 30-36. (in Russian).
 10. Tolkunov I.A. *Bipoliarnaia ionizatsia povitrianogo seredovishcha primishchen funktsionalnykh pidrozdiliv mobilnogo gospitaliu MNS* [Bipolaris ionizationair of air environment of premises of functional units of mobile hospital of the Ministry of Emergencies]. *Problemy nadzvychainykh sytuatsiy* [Problems of Emergencies]. 2014, iss. 14, pp. 161-170. (in Ukrainian).
 11. Tolkunov I.A. and Popov I.I. *Modeliuvannia protsesiv formuvannia poliv kontsetrtsii aeroioniv u povitrianomu seredovishchi prymishchen spetsialnogo pryznachennia MNS Ukrayiny* [Simulation of the process of formation of fields of air ions concentration in the air space of premises the special purpose of the Ministry of Emergencies of Ukraine]. *Problemy nadzvychainykh situatsiy* [Problems of Emergencies]. 2010, iss. 12, pp. 175-184. (in Ukrainian).
 12. Tolkunov I.A., Popov I.I. and Barbasiin V.V. *Teoreticheskoe issledovanie protsessov perenosa ionov v potokakh vozdukh v pomeshcheniyakh spetsialnogo naznacheniya MChS Ukrayiny* [Theoretical study of the ions transfer processes in the air flows in the premises of the special purpose of the Ministry of Emergencies of Ukraine]. *Problemy nadzvychainykh sytuatsiy* [Problems of Emergencies]. 2010, iss. 11, pp. 137-145. (in Russian).
 13. Fletcher L.A., Noakes C.J., Sleigh P.A., Beggs C.B. and Shepherd S.J. *Air ion behavior in ventilated rooms. Indoor and built Environment*. 2008, vol. 17, no. 2, pp. 173-182.
 14. Drexler ., Fiala P. and Bartusek K *Numerical modeling of accuracy of air ion field measurement. Journal of Electrical Engineering*. 2006, vol. 57, no. 8/S, . 62-65.
 15. Murakami, S. *Computational wind engineering. Journal of Wind Engineering and Industrial Aerodynamics*. 1990, vol. 36, part 1, . 517-538.
 16. Noakes C.J., Sleigh P.A. and Beggs C. *Modelling the air cleaning performance of negative air ionizers in ventilated rooms. Proceedings of the 10th International Conference on Air Distribution in Rooms. Roomvent 2007, 13-15 June 2007, Helsinki*. Available at: http://eprints.whiterose.ac.uk/7700/1/Noakes_roomvent_07.pdf. (Accessed 17 September 2015).
 17. Jurelionis A., Gagyt L., Prasauskas T., iužas D., Krugly E., Šeduikyt L. and Martuzevi ius D. *The impact of the air distribution method in ventilated rooms on the aerosol particle dispersion and removal: The experimental approach. Energy and Buildings*. 2015, vol. 86, january, pp. 305-313.

1. - : , 2014. - 136 /
2. - : CFD / , 2015. - 46. -
3. // 168-173.
4. / . . . , , " , , " //
5. 2010. - 19. - 161-168.
5. / . . . , , , , , //
6. / . . . , , , //
- 2011. - 46, 1. - 139-143.
7. / . . . , , // . - 2011. -
. 47, 2. - 120-124.
8. / . . . , , //
- 2012. - 11. - 198-206.
9. . . . , // - 2002. - 1. - 30-36.
10. . . . / //
, 2011. - 14. - 161-170.

11. . . . / . . , . . . //
 / - - , 2010. - . 12. - . 175-184.
12. . . . / . . , . . . , . . . //
 / - - , 2010. - . 11. - . 137-145.
13. Air ion behavior in ventilated rooms / Fletcher L. A., Noakes C. J., Sleigh P. A., Beggs C. B., Shepherd S. J. // Indoor and built environment. – 2008. – Vol. 17, 2. – . 173-182.
14. Drexler . Numerical modeling of accuracy of air ion field measurement / Petr Drexler, Pavel Fiala, Karel Bartusek // Journal of electrical engineering. – 2006. – Vol. 57, 8/S. – . 62-65.
15. Murakami S. Computational wind engineering / S. Murakami // Journal of wind engineering and industrial aerodynamics. – 1990. – Vol. 36, art 1. – . 517-538.
16. Noakes C. J. Modelling the air cleaning performance of negative air ionisers in ventilated rooms / Noakes C. J., Sleigh P. A., Beggs C. // Proceedings of the 10th international conference on air distribution in rooms. Roomvent 2007, 13-15 june 2007, Helsinki, Finland. – : http://eprints.whiterose.ac.uk/7700/1/Noakes_roomvent_07.pdf. – . . . – 17.09.2015.
17. The impact of the air distribution method in ventilated rooms on the aerosol particle dispersion and removal: The experimental approach / A. Jurelionis, L. Gagyt , T. Prasauskas, D. iužas, E. Krugly, L. Šeduikyt , D. Martuzevi ius // Energy and Buildings. – 2015. – Vol. 86, january. – P. 305-313.

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